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Abstract. A wavelength selective wideband uncooled infrared (IR) sensor that detects middle-wavelength and long-wavelength IR (MWIR and LWIR) regions has been developed using a two-dimensional plasmonic absorber (2-D PLA). The 2-D PLA has a Au-based 2-D periodic dimple-array structure, where photons can be manipulated using a spoof surface plasmon. Numerical investigations demonstrate that the absorption wavelength can be designed according to the surface period of dimples over a wide wavelength range (MWIR and LWIR regions). A microelectromechanical system-based uncooled IR sensor with a 2-D PLA was fabricated using complementary metal oxide semiconductor and micromachining techniques. Measurement of the spectral responsivity shows that the selective enhancement of responsivity is achieved over both MWIR and LWIR regions, where the wavelength of the responsivity peak coincides with the dimple period of the 2-D PLA. The results provide direct evidence that a wideband wavelength selective IR sensor can be realized simply by design of the 2-D PLA surface structure without the need for vertical control in terms of gap or thickness. A pixel array where each pixel has a different detection wavelength could be developed for multicolor IR imaging. © The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI. [DOI: 10.1117/1.OE.52.12.127104]

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1 Introduction

There has been increasing interest in the advanced functions of uncooled infrared (IR) image sensors with microelectromechanical system (MEMS)-based pixel structures¹ to expand the applications of IR sensing.² In particular, there is much in a spectral discrimination function that enables uncooled IR sensors to identify objects through their radiation spectrum, which is useful for many applications such as fire detection and gas analysis. A pixel array in which each pixel has a different absorption wavelength could be used to realize multicolor imaging at IR wavelengths, which would provide the same benefits as the RGB pixels of image sensors in the visible region. Therefore, wavelength selectivity is a promising function for an advanced IR sensing.³ Many approaches have been proposed to achieve this, such as band-pass filters,⁴ optical resonant structures,^{5,6} and multilayer structures.⁷⁻¹¹ However, the attachment of external optical systems requires additional space and increases the cost. The optical resonant structures and multilayer structures require gap or thickness control of the dielectric layer to achieve maximum absorption according to the wavelength.^{5,10} Therefore, such typical approaches have difficulty in integrating different pixels in an array for a multicolor imaging.

We have applied plasmonics to address this challenge. A great deal of interest has developed in plasmonics,¹²⁻¹⁴ in which a metal surface structure provides the means for the novel manipulation of photons. Significant advances in the field of photonic crystals¹⁵⁻¹⁷ and micro/nanofabrication techniques have lead to considerable progress in

plasmonics during the last decade. A periodical metal surface structure, referred to as a plasmonic crystal,¹⁸ was reported to have significant potential for the expansion of the operating wavelength region beyond the near-IR region.¹⁹⁻²² Thus, plasmonics is a promising technology for the control of light over a wide spectral range.

Recently, we have reported a wavelength selective uncooled IR sensor that employs plasmonics and functions in the middle-wavelength IR region (MWIR)²³ and partially in the long-wavelength IR region (LWIR).²⁴ However, the wavelength selectivity for both MWIR and LWIR has not yet been reported in detail. In this study, we report the wavelength selectivity of a sensor for both MWIR and LWIR.

2 Design

Figure 1(a) shows a schematic of the Au-based two-dimensional plasmonic absorber (2-D PLA) used as a thermopile, which is a type of uncooled IR sensor. The 2-D PLA has a 2-D periodic array of round dimples on the surface, where photons can be manipulated by spoof surface plasmon polaritons (SPPs).²² Such an asymmetric structure as a one-dimensional grating produces a strong polarization dependency, which is disadvantageous for the IR image sensors. Therefore, a 2-D surface structure with a square lattice and a round dimple was adopted, where only the thin surface metal layer absorbs the incident light.

We have previously reported the absorption properties of a PLA in the MWIR region,²³ where the absorption wavelength was almost the same as the period of the 2-D PLA, due to the spoof SPP mode. The basic design of the Au-based 2-D PLA as an IR absorber for the LWIR at normal incidence was achieved using the rigorous coupled wavelength analysis method. Figure 1(b) shows the wavelength

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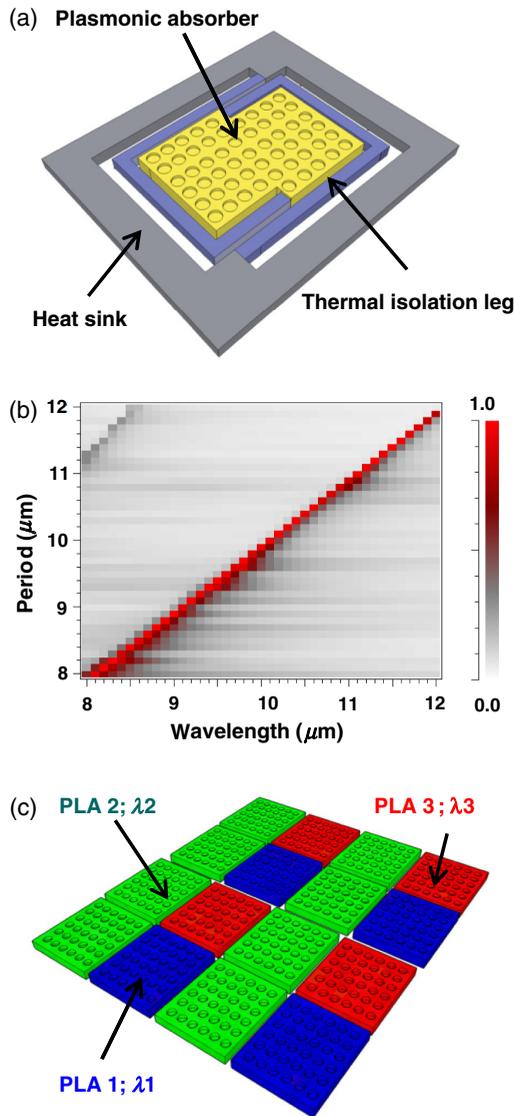


Fig. 1 (a) Schematic diagram of the uncooled IR sensor (thermopile) with Au-based two-dimensional plasmonic absorber (2-D PLA). (b) Calculated wavelength absorption results for the 2-D PLA as a function of the period. (c) Concept of the pixel array with various 2-D PLAs for multispectral imaging.

absorption of the Au-based 2-D PLA as a function of the period from 8.0 to 12.0 μm with a fixed dimple diameter of 6.0 μm and a depth of 1.5 μm . The strong wavelength selective absorption is evident over the LWIR region, as for the MWIR region,²³ and this can be controlled according to the surface period. This satisfies the requirements for an uncooled wideband IR sensor with the wavelength selective function. Figure 1(c) shows the concept of 2-D PLAs with various surface pixel array structures, where three different 2-D PLAs with different absorption wavelengths (λ_1 , λ_2 , and λ_3), were employed. Multicolor imaging can be realized by controlling only the surface structural parameters, such as the dimple period and diameter.

3 Sensor Fabrication

A MEMS-based uncooled IR sensor with 2-D PLAs was developed. The 2-D PLAs are fabricated by forming a Au

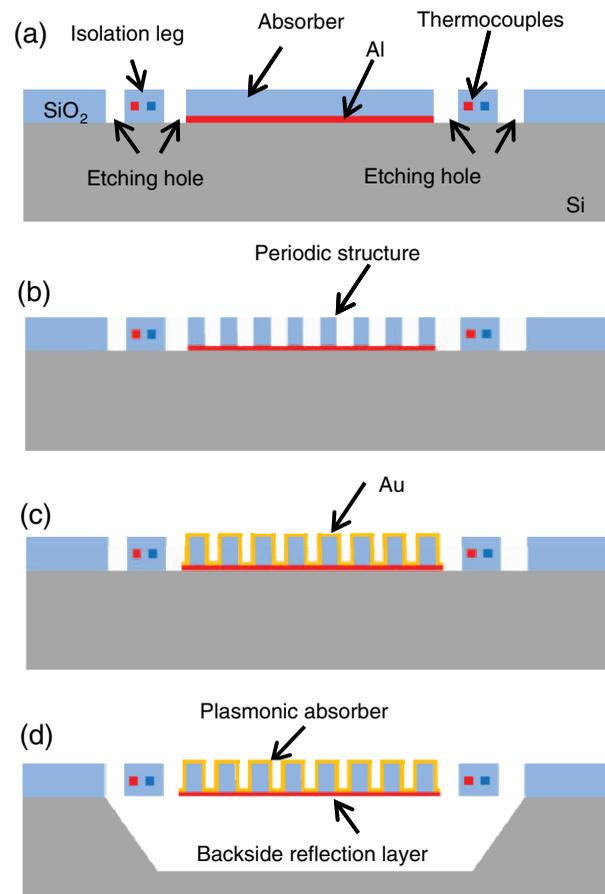


Fig. 2 Schematic diagram of the procedure used to fabricate the MEMS-based thermopile with 2-D PLA. (a) Devices are formed on the surface of a Si wafer using a standard complementary metal oxide semiconductor process. Etching holes are formed by reactive-ion etching. (b) The periodic structure is formed only on the SiO_2 of the IR absorber area by RIE. (c) 50/250-nm thick Cr/Au layers are sputtered, where the Cr layer acts as an adhesion layer between SiO_2 and Au. The 250-nm thick Au layer is sufficiently thicker than the penetration depth in the IR wavelength region, so that absorption by SiO_2 beneath the Au layer is negligible. The Cr/Au layers are selectively etched using a wet etchant to reveal the etching holes covered by

layer on perforated SiO_2 . However, the back side of the SiO_2 layer absorbs scattered light in the LWIR region. To address this issue, an Al layer is introduced to the back side of the 2-D PLA to reflect scattered light. Figure 2 shows the process used to fabricate the MEMS-based thermopile with the 2-D PLA: (a) The devices are fabricated on 6-in p-type Si(1 0 0) substrates using a standard complementary metal oxide semiconductor (CMOS) process. The thermocouples consist of a series of p- and n-types polysilicon, of which the resistivities are controlled by ion implantation. The Al layer is formed as a back side reflection layer under the absorber area. The etching holes for the bulk-micromachining are formed by reactive-ion etching (RIE). A 1.5- μm thick SiO_2 layer is formed on the absorber area. (b) The periodic structure is formed only on the SiO_2 of the IR absorber area by RIE. (c) 50/250-nm thick Cr/Au layers are sputtered, where the Cr layer acts as an adhesion layer between SiO_2 and Au. The 250-nm thick Au layer is sufficiently thicker than the penetration depth in the IR wavelength region, so that absorption by SiO_2 beneath the Au layer is negligible. The Cr/Au layers are selectively etched using a wet etchant to reveal the etching holes covered by

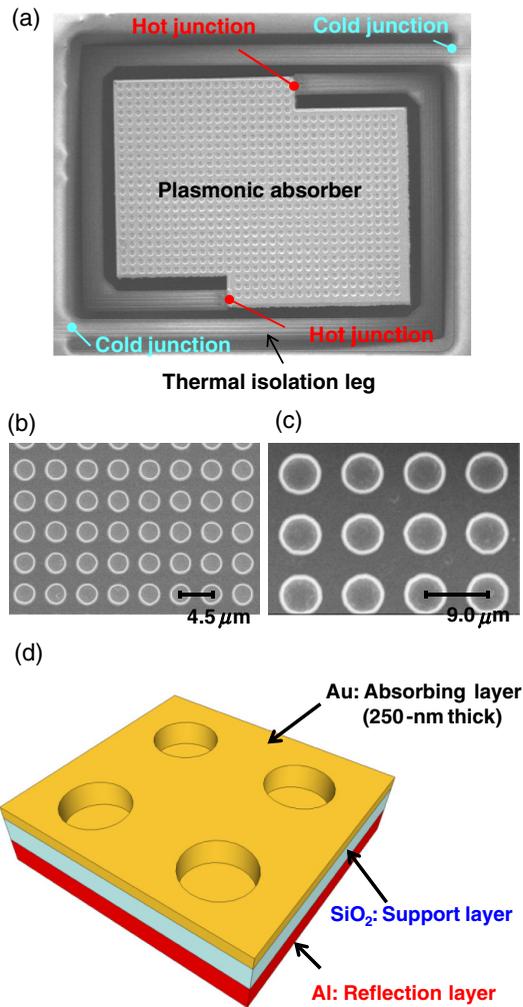


Fig. 3 (a) Scanning electron microscopy (SEM) image of the microelectromechanical system-based thermopile with 2-D PLA developed in this study. Magnified SEM images of the 2-D PLAs of sensors (b) (ii) and (c) (vii). (d) Schematic diagram of the 2-D PLA.

sputtering. Scanning electron microscopy (SEM) observation confirmed that the Cr/Au layers were uniformly coated on both the bottom and side walls of the etched holes to complete the concave Au structure. (d) The wafers are diced into chips. The Si is anisotropically etched using tetramethylammonium hydroxide through the etching holes to form the cavity under the IR absorber area. Finally, a thermally isolated freestanding structure is completed on which the 2-D PLA is formed.

Figure 3(a) shows an SEM image of the developed thermopile. The detector area, which is $300 \times 200 \mu\text{m}^2$, is surrounded by the long thermal isolation legs to reduce the thermal conductance. Various sensors with different 2-D PLA structures were fabricated on the same wafer. The respective diameters and periods of the surface structures were as follows: (i) 3.0 and $4.0 \mu\text{m}$, (ii) 3.0 and $4.5 \mu\text{m}$, (iii) 4.0 and $5.0 \mu\text{m}$, (iv) 4.0 and $6.5 \mu\text{m}$, (v) 6.0 and $7.0 \mu\text{m}$, (vi) 6.0 and $8.0 \mu\text{m}$, (vii) 6.0 and $9.0 \mu\text{m}$, and (viii) 6.0 and $10.5 \mu\text{m}$. The depth was fixed at $1.5 \mu\text{m}$ for all sensors.

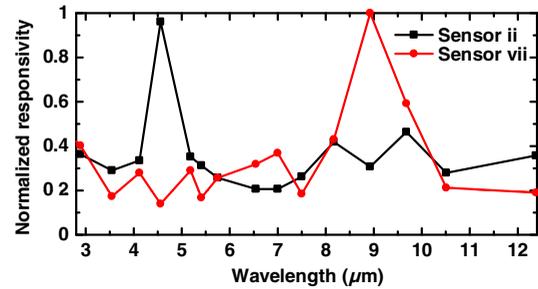


Fig. 4 Measured spectral responsivities for sensors (ii) and (vii).

Figures 3(b) and 3(c) show representative magnified SEM images of two 2-D PLA surfaces. Two periodic structures of 2-D PLA were formed, denoted sensors (ii) and (vii) for MWIR and LWIR, respectively. The diameters and periods of the surface structures of sensor (vii) are linearly twice those of sensor (ii). The depth was fixed at $1.5 \mu\text{m}$ for both sensors. Figure 3(d) shows a schematic of the 2-D PLA structure with the Al reflection layer.

4 Measurements

The wavelength selective properties of the 2-D PLA were investigated. The sensors were set in a vacuum chamber with a Ge window under a pressure of 1 Pa to prevent thermal conduction loss through the atmosphere. The sample was irradiated with IR rays from a blackbody through narrow band-pass filters for the selection of the evaluation wavelengths. The typical full width at half maximum was 80 nm. A pinhole was used to restrict the incident light to the 2-D PLA region only. The output voltage was measured and the responsivity was calculated as the ratio between the output voltage difference of the on and off states and the input power. The input power was calculated according to the measurement system parameters, absorber area, transmittance from the blackbody to the sensor through the atmosphere, narrow band-pass filters and the Ge window, and the spectral radiant emittance equation at the evaluated wavelength as previously reported.²³

The responsivities of sensors (ii) and (vii) were measured first. Figure 4 shows the normalized responsivity of both sensors with clear responsivity peaks in the MWIR and LWIR regions, which coincides with the period of each sensor. The surface structural parameter of sensor (vii) is linearly twice that of sensor (ii) and each sensor has almost the same responsivity. The responsivities of various other sensors were also measured and the results are shown in Fig. 5. The wavelength selectivity was realized for all sensors over a wide range of MWIR and LWIR. The each peak wavelength of responsivity coincides with the periods of each 2-D PLA and these are plotted in Fig. 6 as a function of the surface period of 2-D PLA. These results clearly demonstrate that the detection wavelength is proportional to the surface period; therefore the theory and experimental results are in good agreement.

These results demonstrate that strong absorption occurs due to the spoof SPPs, where responsivity is selectively enhanced and the detection wavelength can be controlled according to the surface period of the 2-D PLA for both MWIR and LWIR regions.

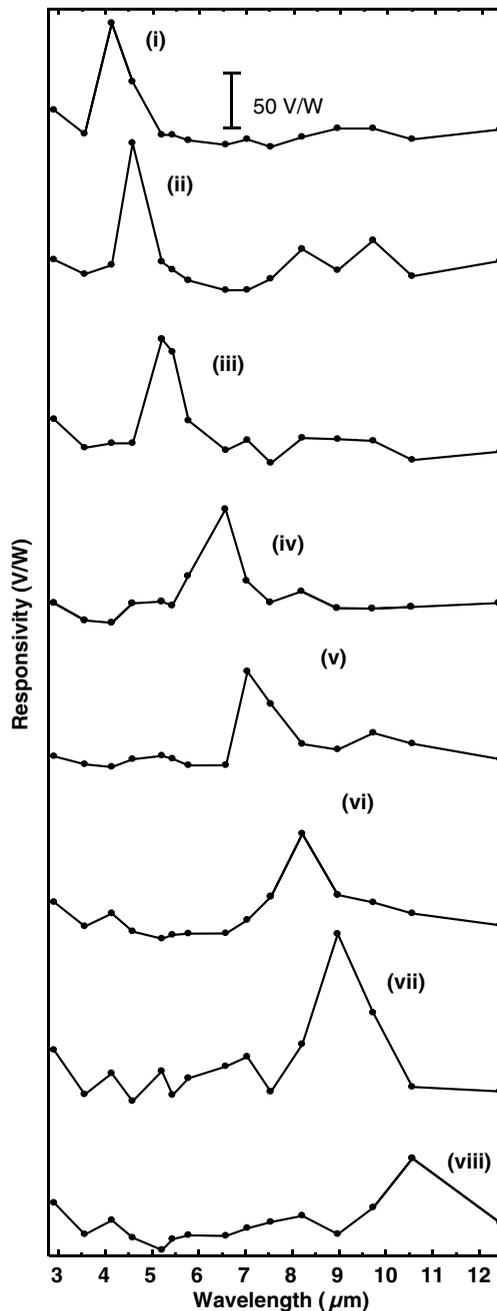


Fig. 5 Spectral responsivity (MWIR and LWIR) for sensors (i)–(viii).

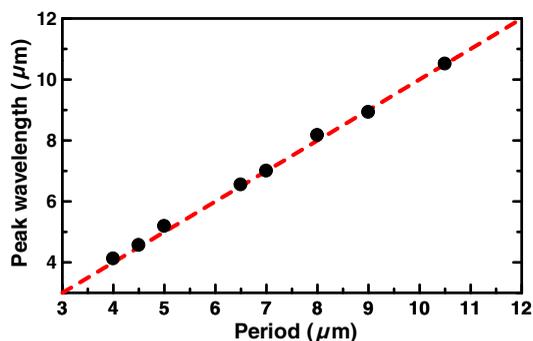


Fig. 6 Peak wavelength of the responsivity as a function of the 2-D PLA surface period.

5 Conclusions

An MEMS-based uncooled IR sensor with 2-D PLAs was fabricated using standard CMOS and micromachining techniques. Responsivity measurements demonstrate that the selective enhancement of the responsivity was achieved over both MWIR and LWIR regions, which is coincident with the period of the 2-D PLA. The obtained responsivities are consistent with the calculated absorption results. These results are direct evidence that the wavelength selective wideband uncooled IR sensor can be realized simply by the design of the 2-D PLA surface structure without the need for filters or multilayer structures. Control of the detection wavelength according to the 2-D PLA can be applied to other types of thermal IR sensors, such as bolometers and silicon-on-insulator diodes.^{25,26} The results presented here should be a significant contribution to the development of novel multicolor imaging for IR sensors.

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